

# PV installation for grid-connected distribution system in Savannakhet Province, Lao People's Democratic Republic

Thavy Khamchaleun<sup>a</sup>, Chayada Surawanitkun<sup>b</sup>, Arkom Kaewrawang<sup>c</sup>

<sup>a</sup>Faculty of Engineering, Khon Kean University, 123 Mittrapharp Road, Khon Kaen 40002, Thailand

<sup>b</sup>Faculty of Applied Science and Engineering, Khon Kaen University, Nong Khai Campus 43000, Thailand

<sup>c</sup>Department of Electrical Engineering, Faculty of Engineering, Khon Kean University 123 Mittrapharp Road, Khon Kaen 40002, Thailand

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## Abstract

Currently, renewable energy is used to connect the grid power system because it is the clean energy and environmental friendly. It is getting worldwide attention such as solar photovoltaic (PV) and is used to generate electricity by stand-alone and grid-connected. The size and the position of the PV are important for installation. Therefore, the aim of this paper is the focus for analysis of PV installation in three positions with the grid-connected distribution system. The PV installation was established by varying capacity of PV considered 100% of the load at 9.46 MW. The DIgSILENT Power-Factory software version 15 was used for system simulation. The voltage in each bus of all cases increases for this analysis. The reactive power flow decreases and reverses to the external grid from 9.46 to -0.27 MW. The current in the 3rd bus to the external grid is reduced from 0.26 to 0.02 kA. The active power losses and reactive power losses are lowest in case of 25-25-50% and 0:50:50%, respectively. This research is the guideline to install the PV for grid-connected with medium voltage system in Lao People's Democratic Republic (Lao PDR) for planning the future policy.

*Keywords: PV generation, distributed generation, power loss, voltage profile*

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## 1. Introduction

In the worldwide, the installed capacity of renewable energy is 2,179,426 MW included the capacity of PV installation – accounted for about 17.9% in 2017 [1]. The manufacturing cost of the PV modules has decreased intensely which it is over \$100 US/W in the 1970s and reduced to under \$1.00 US/W in 2014 [2]. Actually, the price of large-scale PV modules is below \$0.60 US/W [2]. Hence, the PV technology has been developed rapidly in the last decade which effected grown-up to 389.57 GW and it increased to 42 times when compared with 2007 at 9.26 GW [1].

The most of electricity generation in Lao People's Democratic Republic (Lao PDR) is produced from hydropower plants because the location depends on the topography in the country. Mostly, the field of hydropower plant was installed in the northern and southern of the country. However, those energy resources have been installed far from the load which the electrical energy is generated at 11 to 25 kV after that stepped up to 115 kV by the power transformer. It is transferred to the 115/22 kV substation by the long distance that served to domestic, industrial and commercial customers through the distribution transformers. Generally, the power flow in the electricity system of Lao PDR is in one direction from large scale power plants to the end user along the radial feeder. In addition, the 22 kV power network is the type of fishbone. Therefore, the technique losses generated in the transmission line that depends on the length and line impedances of the cable. Furthermore, the voltage drops on the finale feeder. The PV plants popular is used to connect with the low and medium voltage distribution network without energy

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Corresponding author. Tel.: +66(0)43009700 ; E-mail address: arkom@elec.kku.ac.th.

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storage [2]. The advantages of the PV to allow interconnection are maximum benefits because of nearly at the load in the power system, reducing costs of construction and extension of the distribution and transmission lines. Moreover, the appropriate size and location can reduce power losses [3-6]. There are many researchers examined the effects of the high PV penetration level on the medium distribution system, as proposed in the literature [3, 7-10]. The comparison by varying the capacities ratio of PV generators and dissimilar locations for connection to utility grid system is analyzed in literature [5] when the PV is installed in the different buses. It may have to be the positive and negative impacts to the distribution system such as voltage deviations, surplus power flow reversible, energy losses variation, etc [11-12].

The 22 kV of the electric power system in Lao PDR is the long distance. Consequently, there are the power substation and the load demand distribute in the rural area. Savannakhet Province locates in the central part II and the biggest area in Lao PDR. According the annual report of loss reduction and DSM department-technical of EDL reported the average power losses in Savannakhet Province for distribution system (22 kV); in 2018, the power loss is 13.78% (54,602,492 kWh) because the power system has a long length for 22 kV network about 4,173 km over the province. This is the main problem occurred the power loss and the voltage drop in the power system. Therefore, this paper presents the electrical effects on voltage, the active power flow, reactive power flow, current, active power loss and reactive power loss at difference of PV capacity and location for penetration grid connected to the medium power system. Three different locations for PV installation in Savannakhet province are considered for varying the capacity. The DIGSILENT PowerFactory software version 15.1 was used for simulation to analyze the power system.

## 2. Model and Simulation

### 2.1. Savannakhet power system

Savannakhet province is the location in the Central II part of Lao PDR. The electric power grid utility is operated by Electricity DU Laos (EDL) which is the state enterprise company under the Ministry of Energy and Mines. There are five substations in Province's area such as Pakbo, Kengkok, Nongdeun, BanMet (Seno) and MeuangPhin substation. The research methodology selected the actual data from the existing of Savannakhet Province-the 115/22 kV power distribution network of Nongdeun substation was taken into the model. The traditional grid utility consists of 50 MVA transformer step down of 115/22 kV and it has 7 main feeders. The 2nd feeder was chosen in the model simulation because this feeder is the highest peak on the substation as presented in Table 1. The power system contains the 202 buses which are 202 loads, and the 155 kV is the first bus and the 22 kV start from the 2nd to 202nd bus. The power factor at 0.94 is taken into account form model and simulation as shown in Fig. 1 and the capacity of the load presented in Table 2.

Table 1. The peak load annual report of the 2<sup>nd</sup> feeder at Nongdeun substation in 2017

Month	Peak load				Voltage (kV)
	Current (A)	Active power (MW)	Reactive power (MVar)	Power factor	
January	212	7.5	2.98	0.93	23.0
February	167	6.86	2.62	0.92	23.0
March	256	9.13	3.3	0.94	22.0
April	177	6.26	2.53	0.93	23.0
May	241	8.33	3.26	0.93	22.9
June	179	6.31	2.58	0.92	22.5
July	299	8.39	2.56	0.96	23.0
August	177	6.34	2.35	0.94	22.0
September	183	6.62	2.42	0.94	22.8
October	165	5.88	2.38	0.93	22.9
November	215	7.53	3.55	0.9	23.0
December					

## 2.2. System modeling

The existing power grid of urban area in for model simulation was selected. The original case is without the PV. The total load demand is defined by the installed capacity of the transformer. In addition, the steady-state ratio of the capacity of the transformer by the load scale of the 0.285 for active power and the 0.1 for the reactive power are taken into calculated the load factor (LF). The size of the transformers or the loads are divided in the twelve fragments presented in table 2 and the detail of the position of the load is discussed from Ref. [13]. The work specific fixed capacity at 100% of PV installation of the peak load at 9.13 MW in the 2nd feeder of Nongdern power substation. The capacity of the 1st location under 25% is designed three locations: the first at 16°29'21.03" N-104°47'49.39"E, the second at 16°32'7.68" N-104°46'24.52"E and finally at 16°35'36.47" N-104°48'9.76"E were selected. The location of PV 1, 2 and 3 was installed at the 150th, 3rd, and 71st, respectively. The power system was modeled in DlgSILENT PowerFactory software version 15.1 as shown in Fig. 1.

The Aluminum Conductor Steel Reinforced (ACSR) and Space Aerial Cable (SAC) were used in the power system for transport to serve the energy. The size of 240 mm<sup>2</sup> used with the main feeder-the total line length is about 17 km. It transfers the electricity from the 2<sup>nd</sup> to 3<sup>rd</sup> bus and sub-feeder 1 and 2 about 8 km. In addition, the size of 150, 50 and 35 mm<sup>2</sup> were utilized with distributing and branch cables which are the total them length about 32, 28 and 4 km, respectively. The Impedances and line charging reported in Table 3.

Table 2. The loads in the system

Size of transformer	Amount (unit)	Load scale	
		Active power (MW)	Reactive power (MVar)
30	31	0.009	0.003
50	61	0.014	0.005
100	36	0.028	0.010
160	31	0.046	0.016
250	25	0.071	0.026
315	6	0.090	0.032
400	5	0.114	0.041
500	1	0.142	0.051
630	1	0.179	0.065
1000	1	0.285	0.103
1250	1	0.356	0.129
2000	3	0.570	0.206

Table 3. Impedances and line charging of the cable [14]

Size (mm <sup>2</sup> )	Z1 (Ω/km)		Z0 (Ω/km)		B0 (μS/km)	B1 (μS/km)	Current Rating (A)
	R1 (Ω/km)	X1 (Ω/km)	R0 (Ω/km)	X0 (Ω/km)			
ACSR 25	1.138	0.4818	1.3158	1.9333	1.49	3.45	145
ACSR 35	1.11	0.4129	1.2582	1.6397	1.26	2.97	126
ACSR 50	0.556	0.3912	0.7042	1.6180	1.29	3.15	190
ACSR 150	0.1830	0.3281	0.3312	1.5550	1.34	3.47	335
ACSR 240	0.1343	0.3179	0.2825	1.5448	1.36	3.60	560
SAC 240	0.125	0.327	0.2732	1.5538	1.34	3.48	525

## 2.3. Analysis of the Power Flow

Load flow analysis in power system is important to evaluate power flow problems and planning. The relation of node current and voltage in the power system on the linear network can be presented by Newton-Raphson equation [15]

$$I = Y_{bus} V \quad (1)$$

or

$$I_i = \sum_{j=1}^N Y_{ij} V_j \quad (i = 1, 2, 3, \dots, n) \quad (2)$$

where  $I_i$  is the injected current for bus  $i$  and  $V_j$  is the voltage for bus  $j$ . The  $Y_{ij}$  is the element of the admittance and  $n$  is the total number of nodes in the power system.

The solution of load flow problem by used the equation, should be used the relation between the node power and the current, which can be calculated by

$$I = \frac{P_i - jQ_i}{\hat{V}_i} \quad (i = 1, 2, 3, \dots, n) \quad (3)$$

where  $P_i$  is the active power and  $Q_i$  is the reactive power at node  $i$ , in case node  $i$  is a load node in the system. Therefore,  $P_i$  and  $Q_i$  are take the negative values and  $\hat{V}_i$  is the conjugate of the voltage vector at node  $i$  in the network. The injected current can be summarized as eq. (4).

$$\frac{P_i - jQ_i}{\hat{V}_i} = \sum_{j=1}^N Y_{ij} V_j \quad (i = 1, 2, 3, \dots, n) \quad (4)$$

$$S_i = \sum_{k=1}^n |V_i| |V_k| (\cos \theta_{ik} + j \sin \theta_{ik}) (G_{ik} - jB_{ik}) \quad (i = 1, 2, 3, \dots, n) \quad (5)$$

where  $S_i$  is the apparent power and  $\theta_{ik}$  is the phase angle between bus  $i$  and bus

$$P_i = \sum_{k=1}^n |V_i| |V_k| (G_{ik} \cos \theta_{ik} + B_{ik} \sin \theta_{ik}) \quad (6)$$

$$Q_i = \sum_{k=1}^n |V_i| |V_k| (G_{ik} \sin \theta_{ik} - B_{ik} \cos \theta_{ik}) \quad (7)$$

where  $P_i$  is the active power and  $Q_i$  is the reactive power at node  $i$ , the  $\hat{V}_i$  and  $\hat{V}_k$  is the conjugate of the voltage vector at node  $i$  and  $k$  in the network, respectively. The  $G_{ik}$  and  $B_{ik}$  are called conductance and susceptance, respectively.

For analysis of the power losses in distribution systems, there are two major sources that are in the power lines and transformers.

$$P_{Loss} = I^2 R \quad (8)$$

$$Q_{Loss} = I^2 X \quad (9)$$

where  $R$ ,  $I$  and  $X$  are resistance, current and reactance of the conductor, respectively.



### 3. Results and Discussions

#### 3.1. Power flow feed in external grid

The power flow in the original case (without PV) is one-way flow from the external grid to the load such as the active power and reactive power are 9.46 MW and 4.22 MVar, respectively. Then, the PV was connected in the power system. The results show that the power flow reverses to external grid at the rang from -0.03 to -0.27 MW for active power because the it generates from the PV source to supply the load effected reduce power loss. In addition, the reactive power reduces from 4.22 to 3.39 MVar as demonstrated in the Table 4.

Table 4 Total power losses for variable cases of the PV installation

Location of installed PV	study cases	External Infeed	
		Active power (MW)	Reactive power (MVar)
Without PV	0%	9.46	4.22
1	100:0:0%	-0.03	3.92
2	0:100:0%	-0.21	3.51
3	0:0:100%	-0.22	3.48
1-2-3	25:25:50%	-0.27	3.39
1-2-3	0:50:50%	-0.27	3.4
1-2-3	0:25:75%	-0.26	3.41
1-2-3	25:0:75%	-0.26	3.41
1-2-3	0:75:25%	-0.25	3.43
1-2-3	25:50:25%	-0.25	3.42
1-2-3	25:75:0%	-0.21	3.5

#### 3.2. The voltage magnitude the difference location and capacity of

Fig. 2 shows the voltage in original case (0%), the analysis results found the voltage lowest on the 101st bus at 0.976 p.u. because of the end of feeder I and heavy load. It increases on the 102nd bus at 0.995 p.u. because this bus direct connects with the 4th bus. In addition, on the 133rd bus the voltage value rises to 0.997 p.u. because it links with the 3rd bus and it is the first bus on the sub-feeder II. In the final bus of the 2nd sub-feeder the voltage drops to 0.982 p.u. After that, the PV was installed on the 3rd, 71st and 150th bus accordingly the PV variation by different percentage at 100% of the peak load at 9.31 MW. The effect occurred in the power system. The voltage level at all the buses over the 1 p.u. but under the 1.05 p.u. However, it is still in standards range of rated voltage for normal operating and emergency conditions is defined the voltage deviation, the rang of  $\pm 5\%$  and  $\pm 10\%$  of the voltage deviation [16-17].

#### 3.3. The active and reactive power losses

The power loss in the original case found the both active and reactive power losses at 0.32 MW and 0.9 MW, respectively. It occurred from a lot of factors such as the power line in this feeder was used ACSR 150 (high resistance), long distant, PV generated over the load, joule heat in the line. Next, The PV was installed by different ratio and according the location. The lowest power loss is found in the case integrated PV from three sites for PV installation as well as the ratio is 25:25:50 of location 1, 2 and 3, respectively, due to the PV generation sources distributed near the load. Thus, the power transmission is short length. In addition, once case the same value for active power reactive power is 50:50% of location 2 and 3, respectively, as shown in Fig. 3.

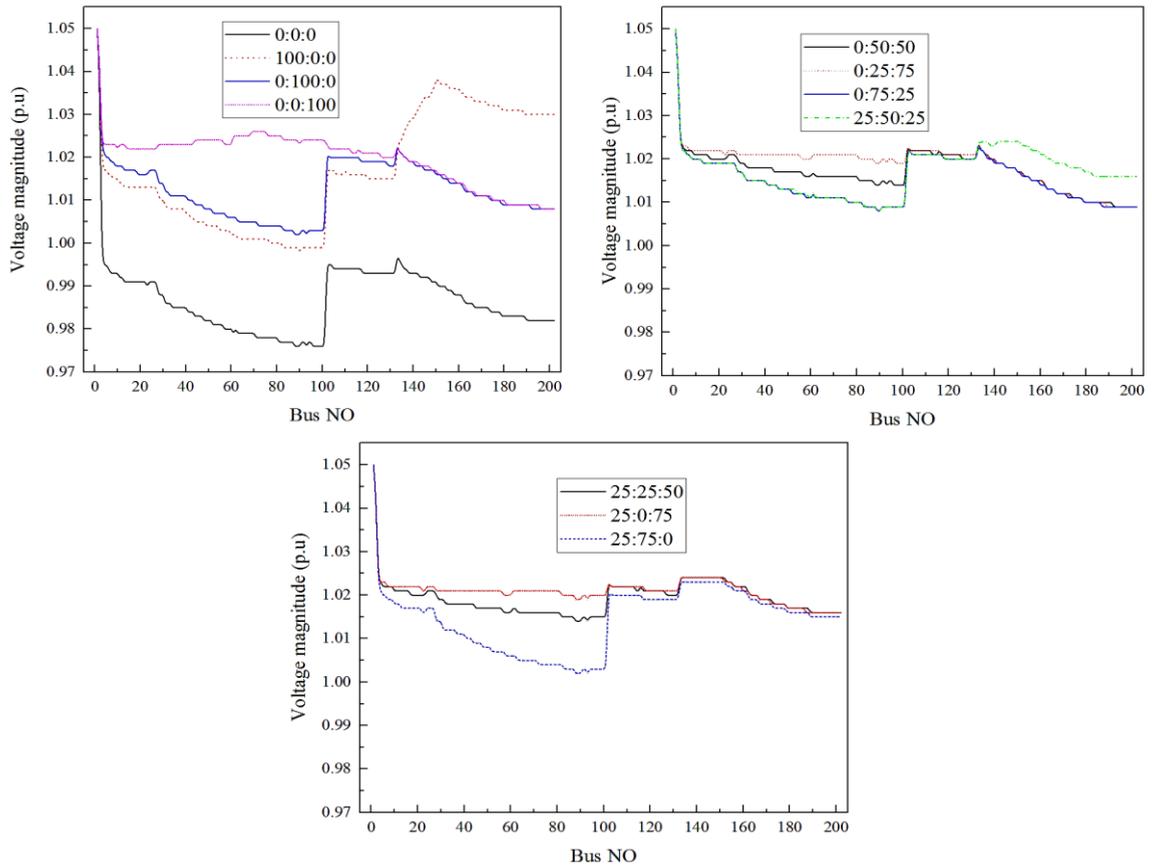


Fig. 2. The voltage magnitude variation in each bus when the PV connected to the grid

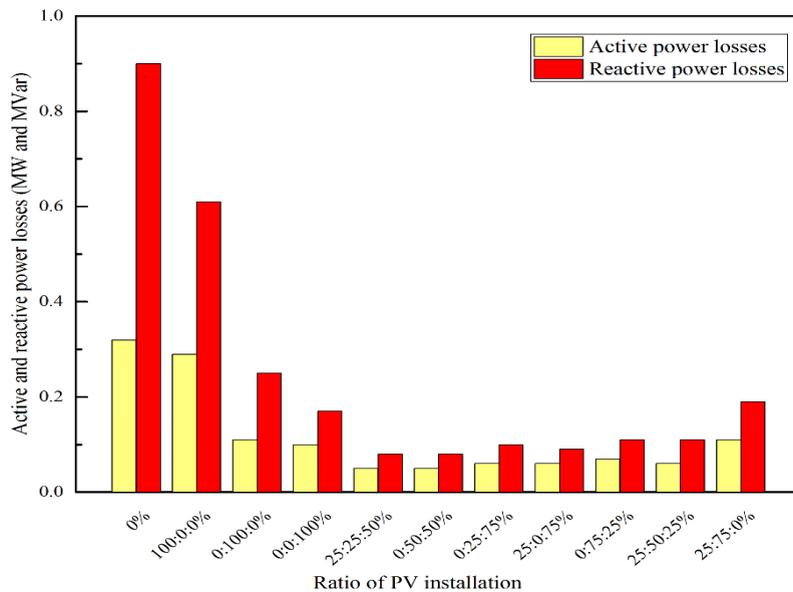


Fig. 3 The Active and reactive power losses at different percentages of the PV installation in the three location

### 3.4. The current

The current from 3<sup>rd</sup> bus to 202<sup>nd</sup> bus is the constant value but it deviates the flow direction because it generates from the PV to deliver the load. On the other hand, it decreases from the 3<sup>rd</sup> bus to external grid such as 0.26 to 0.02 kA. This leads to overcurrent in the system that some part of current movement outside of the area.

## 4. Conclusions

This paper presents the effects of size PV installation with utility grid connected on PV power distribution system in Savannakhet Province. The PV was installed in three locations that varied the capacity size of the PV at 100% in 2<sup>nd</sup> feeder in Nongdorn power substation. The 11 cases of varying ratio of the PV size are without PV, 100:0:0, 0:100:0, 0:0:100, 25:25:50, 0:50:50, 0:25:75, 25:0:75, 0:75:25, 25:50:25 and 25:75:0%. The results show the voltage in all case when the PV was installed in the power system. The active power loss and reactive power loss are minimum in both case at 25:25:50 and 0:50:50. In addition, the current decreases in the 3<sup>rd</sup> bus to external grid. Moreover, the active power reverses to the external grid. The results in this study are useful to apply the renewable energy in the power system with PV installation.

## Conflict of Interest

The authors declare no conflict of interest.

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