

Power loss reduction and reliability improvement of a large-scale electrical distribution system using network reconfiguration

Arun Onlam, Daranpob Yodphet, Apirat Siritaratiwat, Rongrit Chatthaworn ,
Chayada Surawanitkun and Pirat Khunkitti *

Department of Electrical Engineering, Faculty of Engineering, Khon Kaen University 40002, Thailand.

Abstract

Network reconfiguration of an electrical distribution system is an outstanding technique to improve the performance of a distribution system. The main factors indicating the performance of the system are the electrical power loss and the system reliability. In this paper, the multi-objective reconfiguration of a large-scale electrical distribution system located in Khon Kaen province, Thailand is proposed by using the Enhanced Genetic Algorithm. The total electrical power loss, system average interruption frequency index, system average interruption duration index, energy not supplied and the total cost are analyzed as the objective functions. The results show that the power loss of the illustrative system is significantly reduced as compared to the initial configuration. Furthermore, the reliability indices of the distribution system can be improved, while the total cost is decreased. Thus, it is indicated that the overall performance of the particular distribution system is significantly improved after network reconfiguration, which can be utilized for distribution system expansion planning.

Keywords: multi-objective function reconfiguration, genetic algorithm, optimal total cost, optimal distribution power system

1. Introduction

In electrical distribution systems, electrical power loss and system reliability are the main factors indicating the performance of the system [1]. Meanwhile, economic factors for the system also need to be carefully optimized, as it is widely known that these factors depend mainly on the power loss of the system. The network reconfiguration of electrical distribution systems is one effective technique to improve the performance of the system, i.e. power loss reduction, reliability improvement, load balancing, enhanced benefit/cost ratio, switching maneuvers and voltage profile enhancement [2]. The network reconfiguration is a procedure that changes the status of tie-line and section switches, which can alter the electrical power flow of the system. Since the load demand of the distribution system is always changing over time, this procedure can essentially handle the system alternation.

Several procedures have been proposed for optimizing reconfiguration problems, which are mostly multi-objective with nonlinear scale. The meta-heuristic methods are extensively known to be effective methods for solving those problems; the main advantage of these methods is their robust search of the solution space [3]. Many meta-heuristic algorithms have been proposed to solve the network reconfiguration problem for both single objective and multi-objectives, such as the Genetic Algorithm (GA), the Ant Colony Search Algorithm (ACSA) [3], the Simulated Annealing Algorithm (SA) [4], Tabu Search (TS) [5], Particle Swarm Optimization (PSO) [6], the Shuffled Frog Leaping Algorithm (SFLA) [7], and Honey Bee Mating Optimization (HBMO) [8].

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Corresponding author. Tel.: +66-86-636-5678; E-mail address: piratk@kku.ac.th.

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In particular, GA has been one of the common methods used to solve optimization problems. The advantage of this algorithm is its ability to efficiently solve for discrete variables and non-linear, non-differential, non-continuous problems. However, there are still some limitations to GA to solve a large-scale electrical distribution system problem, due to the complexity and the radial topology constraints of the systems [9-12]. Accordingly, several methods based on GA have been developed to overcome these limitations, i.e. the Adaptive Genetic Algorithm (AGA) and the Enhanced Genetic Algorithm (EGA) [13, 14]. The AGA is appropriate for solving the multi-objective reconfiguration of distribution systems. The idea of this method is to improve the circumstances of all nodes connected to a power supply, and avoid searching for isolated interior nodes by creating the feasible individuals using graph theory, which results in a short computational time with optimal solutions. Nevertheless, in a large-scale electrical distribution system, system complexity is still the main problem for the AGA. Then, D.-L. Duan et al. proposed the EGA by applying the Kruskal graph theory to the crossover operation of the GA. It was found that the EGA method could guarantee a radial topology of the distribution system, and avoid the tedious mesh checking. Therefore, the EGA has become an appropriate algorithm for solving a complicated electrical distribution system problem.

In this paper, we propose the network reconfiguration for an electrical distribution system by using the EGA. A practical distribution system in Khon Kaen province, Thailand is used in the reconfiguration. The multiple objectives of the network reconfiguration include electrical power loss reduction and reliability improvement. The reliability indices focused on are system average interruption frequency index (SAIFI), system average interruption duration index (SAIDI) and energy not supplied (ENS). The MATLAB program is utilized in the simulations.

2. Problem Formulation

The multi-objective electrical distribution system reconfiguration is to minimize the real power loss while maximizing the reliability indices under various operating constraints. The electrical system is considered as a balanced three-phase load, while all loads are assumed as constant power loads. Each objective function is formulated as below.

2.1. Real power loss of distribution systems

The real power loss of distribution systems is expressed as (1),

$$P_{loss} = \sum_{i=1}^n \frac{R_i (P_i^2 + Q_i^2)}{V_i^2} \quad (1)$$

subject to the following constraints:

$$- I_i \leq I_i^{\max} \quad (2)$$

$$- V_{\min} \leq V_i \leq V_{\max} \quad (3)$$

$$- g_i(I, k) = 0, g_v(V, k) = 0 \quad (4)$$

where R_i is the resistance of the i^{th} branch, P_i, Q_i, I_i and V_i are real power, reactive power, current magnitude and voltage at the sending end of the i^{th} branch, respectively. I_i^{\max} , V_{\min} and V_{\max} are maximum current, minimum voltage and maximum voltage, respectively, while $g_i(I, k), g_v(V, k)$ represent Kirchhoff's voltage and current laws, respectively.

2.2. Reliability indices of electrical distribution system

As mentioned above, the reliability indices used to evaluate the electrical distribution system reliability are SAIFI, SAIDI and ENS [2]. These indices are generally used to indicate the performance of a

distribution system when transmitting continuous electrical power to all customers. The SAIFI, SAIDI and ENS can be calculated as in the following equations.

$$SAIFI = \frac{\sum \lambda_i N_i}{\sum N_i} \quad (5)$$

$$SAIDI = \frac{\sum U_i N_i}{\sum N_i} \quad (6)$$

$$ENS = \sum_{i=1}^N L_{avg(i)} U_i \quad (7)$$

where λ_i is the system failure rate per year at load point i , U_i is the annual outage duration per year at load point i , N_i is the total number of consumers at load point i and $L_{avg(i)}$ is the average load connected to load point i .

2.3. Total lost cost

Another important objective function for the network reconfiguration is to minimize the total cost of the system. In this work, the total cost includes the total lost cost, utility cost and customer interruption cost, as expressed in (8). It is noted that the utility cost is the cost lost during system operation and when a failure occurs, while the customer interruption cost is the cost lost when the electrical supply is interrupted. The total lost cost can be written as (8),

$$TC = TLC + UIC + CIC / kWh + CIC / Time \quad (8)$$

where TC denotes the total cost for the electrical distribution system. The cost of annual power loss (TLC) can be expressed as follow [15]:

$$TLC = C_p \sum_{d=1}^{365} \sum_{t=1}^{24} P_{loss} \quad (9)$$

where C_p represents the energy cost (Thai Baht/kWh). P_{loss} is defined as the power loss.

When an interruption occurs in the electrical distribution system, where the power supply utility and customer use are interrupted, the utility interruption cost (UIC) can be derived as follows [16],

$$UIC = C_p \times ENS \quad (10)$$

CIC / kWh is defined as the customer interruption cost per kilowatt-hour, given as [17],

$$CIC / kW = ENS \times IEAR \quad (11)$$

where $IEAR$ is defined as the interrupted energy assessment with the rate of 60.165 Thai Baht/kWh.

$CIC / Time$ is defined as customer interruption cost per time, *UtilityCost* and *CustomerOutageCost* are defined as total utility cost and total costumer outage cost written as follows [17]:

$$CIC / Time = SAIFI \times ICPE \quad (12)$$

$$UtilityCost = TLC + UIC \quad (13)$$

$$CustomerOutageCost = CIC / kWh + CIC / Time \quad (14)$$

where $ICPE$ is defined as the interruption cost per event (62,723 Thai Baht/time).

3. Reconfiguration Procedures of an Electrical Distribution System

In the network reconfiguration of the Khon Kaen electrical distribution system, the EGA is used to solve this problem due to its outstanding properties for solving large-scale systems. The EGA is initialized with a population size of 30 and a maximum generation of 100. As shown in Fig. 1, the procedure for the EGA can be summarized into 7 steps, as follows [12-14]:

Step 1: Read data about the distribution system to define a loop vector population by codification. Then, formulate common branch vectors and prohibited group vectors using graph theory.

Step 2: Generate the initial population with the fitness function.

Step 3: Select two individuals as parents by the selection operation using tournament selection.

Step 4: Search for optimal solutions for the set of open switches by updating the generations with the crossover process. This operation is modified by the Kruskal theory to create a descendant.

Step 5: Check for violated rules of the radial topology and correct using the loop vector, common branch vectors and prohibited group vectors.

Step 6: Characterize the load flow and reliability.

Step 7: Repeat steps 3-6 until the number of iterations is satisfied.

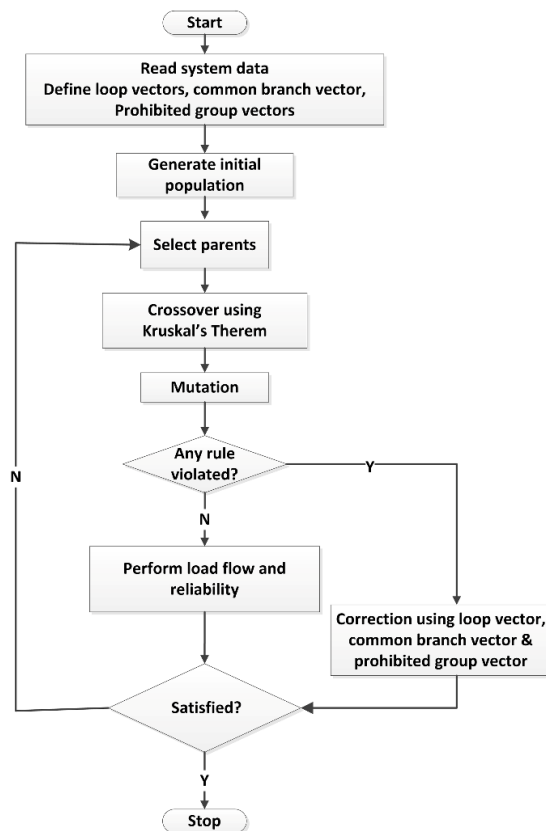


Fig. 1. Overview of the procedure for the EGA algorithm

4. Reconfiguration Results for Khon Kaen Electrical Distribution System

Fig. 2 shows the practical distribution system for Khon Kaen province, Thailand consisting of 123 buses with 144 branches. The rated voltage of this system is 22 kV. The power system and reliability data of this particular distribution system are indicated in **Appendix A**. In the simulations, it is assumed that the load data has a constant value; the total active load power is 87.28 MW with 45.98 MVAR reactive load power. The initial power loss of this system is 1,454 kW. The loss factor of 0.76 is also included in the calculations, which is obtained from the load factor of the practical distribution system. The number of initial normally open switches of the distribution system is 22, which will be equal to those after reconfiguration.

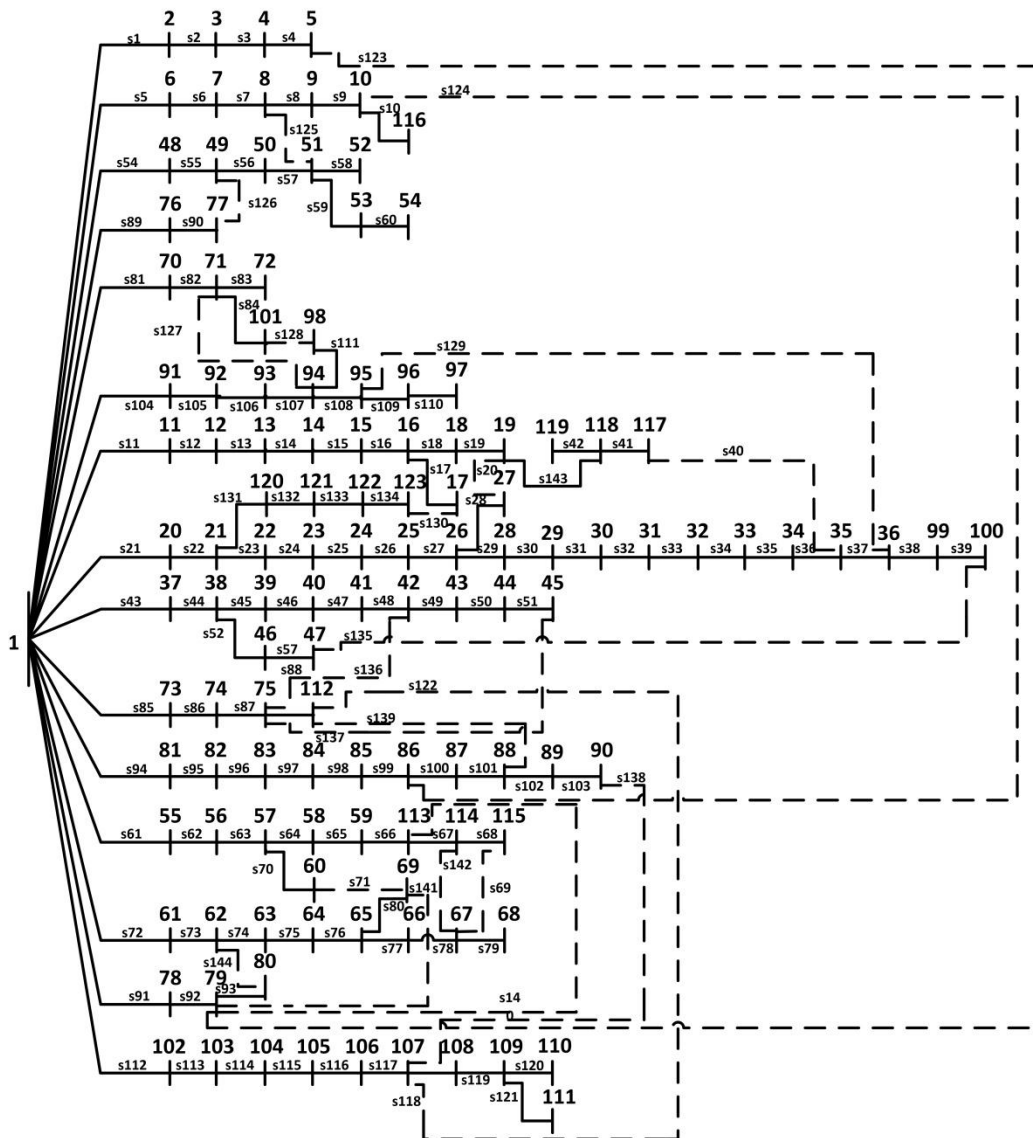


Fig. 2. The practical 123-bus distribution system in Khon Kaen province, Thailand

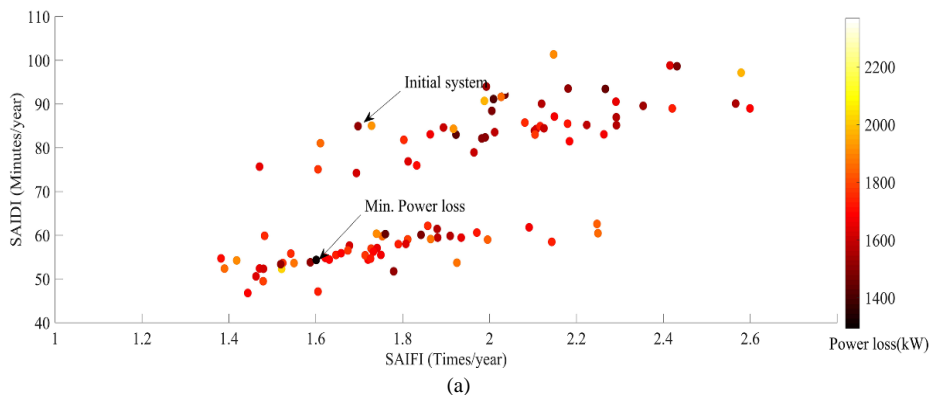
The simulation results for the network reconfiguration are shown in Table 1. The objective functions indicated in each row of the table include total power loss (kW), SAIFI (T/Y), SAIDI(M/Y), ENS (Kwh),

utility cost (Baht), customer outage cost (Baht), total cost (Baht) and opened switches. Meanwhile, the focused objective functions are indicated as 4 cases in each column, including min. total power loss (case 1), min. SAIFI (case 2), min. SAIDI (case 3) and min. total cost (case 4). As shown in Table 1, the total power losses, SAIFI, SAIDI, ENS and the total cost in case 1 are less than those of the base case. In case 2 and case 3, it is seen that SAIFI, SAIDI, ENS are less than the base case, whereas the total power loss and the total cost are lower than the base case. Similarly to case 1, the total power losses, SAIFI, SAIDI, ENS and the total cost in case 4 are less than the those of the base case. In addition, ENS in every case has decreased from the base case. It was found that case 1 indicates the minimum utility cost. This is because the power loss has the most significant impact on the utility cost. Moreover, the customer outage cost is decreased from the base case in every case due to a reduction of SAIFI and ENS.

From the above discussions, it is concluded that the objective functions in case 1 and case 4 can provide the best results for network reconfiguration, because overall worthiness of the system is improved from the base case. In particular, it is found that the total power loss, the total cost, SAIFI and SAIDI of case 1 and case 4 are reduced about 11.02%, 12.15%, 3.6% and 53.33 % from the base case, respectively.

Table 1. Optimal solutions of network reconfiguration results with different objectives.

| Focused objective function | Initial configuration (Base case) | Min. total power loss (case 1) | Min. SAIFI (case 2) | Min. SAIDI (case 3) | Min. total cost (case 4) |
|-----------------------------|---|--|--|--|--|
| Total power loss (kW) | 1,454.60 | 1,294.25 | 1,884.69 | 1,729.74 | 1,294.25 |
| SAIFI (times/year) | 1.66 | 1.60 | 1.33 | 1.53 | 1.60 |
| SAIDI (minutes/year) | 86.28 | 54.33 | 56.79 | 50.49 | 54.33 |
| ENS (Kwh) | 82,682.51 | 64,827.23 | 70,013.62 | 68,466.77 | 64,827.23 |
| Utility cost (Baht) | 43,504,888.61 | 38,679,532.33 | 56,242,281.03 | 51,632,492.32 | 38,679,532.33 |
| Customer outage cost (Baht) | 5,079,026.21 | 4,000,749.69 | 4,295,889.15 | 4,215,279.82 | 4,000,749.69 |
| Total cost (Baht) | 48,583,914.82 | 42,680,282.02 | 60,538,170.18 | 55,847,772.14 | 42,680,282.02 |
| Opened switches. | 20,40,69,71, 122,123,124,125, 126,127,128,129, 130,135,136,137, 139,138,140,144, 142, 144 | 17,19,35,41, 47,51,65,67, 68,80,100,103, 111,122,123,124, 125,126,127,135, 141,144 | 8,19,26,29, 38,50,57,67, 80,87,90,100, 103,106,122,123, 127,130,140,141, 142,144 | 9,26,32,38, 40,64,69,76, 80,89,103,107, 111,115,123,125, 131,136,137,139, 141, 144 | 17,19,35,41, 47,51,65,67, 68,80,100,103, 111,122,123,124, 125,126,127,135, 141,144 |



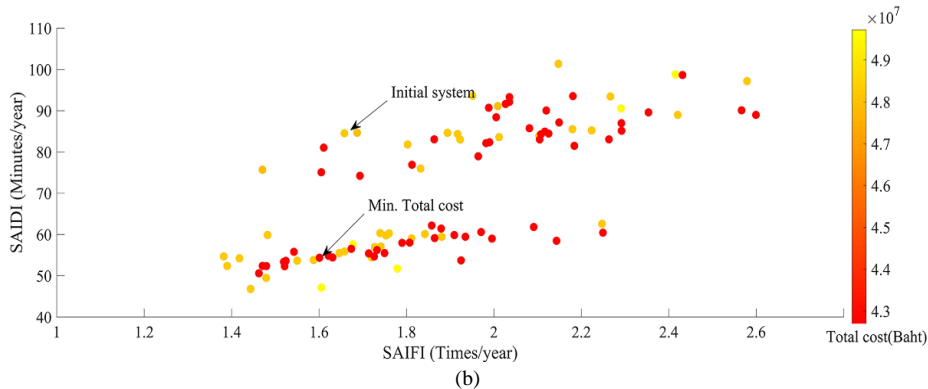


Fig. 3. Relationships between SAIDI and SAIFI and different values of (a) power loss and (b) total cost

Figs. 3(a) and 3(b) show the relationships between SAIDI and SAIFI for different values of power loss and total cost, respectively. When focusing on minimum power loss and minimum total cost as the objective functions, it is found that the power loss and the total cost of the system can be significantly reduced from the initial value, while the reliability indices of the system are increased. Also by focusing on the minimum SAIFI or minimum SAIDI, the system reliability can be improved from the initial configuration. However, the power loss of the system in these cases is increased. It is thus concluded that the minimal power loss and minimal total cost are the most suitable objective functions for the network reconfiguration of this particular distribution system.

5. Conclusion

In this paper, the multi-objective reconfiguration of a large-scale electrical distribution system of Khon Kaen province, Thailand is presented in order to improve the performance of the distribution system. We focused on four objectives being minimized total power loss, minimized SAIFI, minimized SAIDI and minimized total cost under distribution system constraints. It was found that the optimal solution for the network reconfiguration of this system occurs when the minimized total power loss and minimized total cost are optimized. The results show that the total power loss, total cost, SAIFI and SAIDI of the reconfigured system are reduced by 11.02%, 12.15%, 3.6% and 53.33 % respectively from the initial configuration. Moreover, the pareto front indicates that when the minimized power loss and total cost occur, the reliability indices of the distribution system can be significantly improved. However, the system analysis indicates more total power loss than the initial value when the minimized reliability indices are focused on. From the results, it is seen that the overall performance of this particular system can be improved by network reconfiguration, which also reduces the expenses regarding system operation. The results can also be used to provide optimal solutions for network planning for further system expansion.

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Appendix A:

Table A.1 Power system and reliability data of a distribution system in Khon Kaen province, Thailand.

| Branch No. | Fbus | Tbus | R | X | Failure rate (Times/Year) | Duration Time (Minutes/Year) | Bus No. | P Load (kW) | Q Load (kVar) | No. Customers |
|------------|------|------|--------|--------|---------------------------|------------------------------|---------|-------------|---------------|---------------|
| 1 | 1 | 2 | 0.0000 | 0.0007 | 2.33 | 118 | 1 | 0.000 | 0.000 | 0 |
| 2 | 2 | 3 | 0.1345 | 0.1906 | 2.33 | 118 | 2 | 0.000 | 0.000 | 0 |
| 3 | 3 | 4 | 0.2146 | 0.3061 | 2.33 | 118 | 3 | 0.491 | 0.259 | 1,227 |
| 4 | 4 | 5 | 0.0245 | 0.0866 | 2.33 | 118 | 4 | 1.779 | 0.937 | 2,000 |
| 5 | 1 | 6 | 0.0000 | 0.0006 | 3.33 | 81.33 | 5 | 2.402 | 1.265 | 2,773 |
| 6 | 6 | 7 | 0.1165 | 0.1651 | 3.33 | 81.33 | 6 | 0.000 | 0.000 | 0 |
| 7 | 7 | 8 | 0.0840 | 0.1191 | 3.33 | 81.33 | 7 | 1.964 | 1.035 | 374 |
| 8 | 8 | 9 | 0.1749 | 0.2479 | 3.33 | 81.33 | 8 | 0.424 | 0.224 | 5 |
| 9 | 9 | 10 | 0.0927 | 0.1314 | 3.33 | 81.33 | 9 | 0.906 | 0.477 | 1,460 |
| 10 | 10 | 116 | 0.2381 | 0.3375 | 3.33 | 81.33 | 10 | 3.048 | 1.606 | 1,388 |
| 11 | 1 | 11 | 0.0001 | 0.0014 | 0.33 | 7.33 | 11 | 0.000 | 0.000 | 0 |
| 12 | 11 | 12 | 0.0869 | 0.1231 | 0.33 | 7.33 | 12 | 1.714 | 0.903 | 142 |
| 13 | 12 | 13 | 0.0020 | 0.0029 | 0.33 | 7.33 | 13 | 0.000 | 0.000 | 0 |
| 14 | 13 | 14 | 0.0085 | 0.0120 | 0.33 | 7.33 | 14 | 0.166 | 0.087 | 2 |
| 15 | 14 | 15 | 0.0032 | 0.0045 | 0.33 | 7.33 | 15 | 0.000 | 0.000 | 0 |
| 16 | 15 | 16 | 0.0035 | 0.0049 | 0.33 | 7.33 | 16 | 0.788 | 0.415 | 4 |
| 17 | 16 | 17 | 0.0117 | 0.0165 | 0.33 | 7.33 | 17 | 0.139 | 0.073 | 4 |

| 30 | 28 | 29 | 0.0001 | 0.0013 | 1.67 | 34.33 | 30 | 0.000 | 0.000 | 0 |
|------------|------|------|--------|--------|---------------------------|------------------------------|---------|-------------|---------------|---------------|
| 31 | 29 | 30 | 0.0000 | 0.0009 | 1.67 | 34.33 | 31 | 0.082 | 0.043 | 25 |
| 32 | 30 | 31 | 0.0000 | 0.0000 | 1.67 | 34.33 | 32 | 0.000 | 0.000 | 0 |
| 33 | 31 | 32 | 0.0000 | 0.0000 | 1.67 | 34.33 | 33 | 0.000 | 0.000 | 0 |
| 34 | 32 | 33 | 0.0000 | 0.0004 | 1.67 | 34.33 | 34 | 0.255 | 0.134 | 1 |
| 35 | 33 | 34 | 0.0000 | 0.0010 | 1.67 | 34.33 | 35 | 0.000 | 0.000 | 0 |
| 36 | 34 | 35 | 0.0000 | 0.0006 | 1.67 | 34.33 | 36 | 4.139 | 2.180 | 642 |
| 37 | 35 | 36 | 0.0005 | 0.0092 | 1.67 | 34.33 | 37 | 0.000 | 0.000 | 0 |
| 38 | 36 | 99 | 0.0183 | 0.0260 | 1.67 | 34.33 | 38 | 2.771 | 1.460 | 1,454 |
| 39 | 99 | 100 | 0.0138 | 0.0195 | 1.67 | 34.33 | 39 | 0.734 | 0.387 | 685 |
| 40 | 35 | 117 | 0.0360 | 0.0510 | 1.67 | 34.33 | 40 | 0.872 | 0.459 | 1,242 |
| 41 | 117 | 118 | 0.0055 | 0.0078 | 1.67 | 34.33 | 41 | 0.016 | 0.008 | 2 |
| 42 | 118 | 119 | 0.0378 | 0.0535 | 1.67 | 34.33 | 42 | 0.480 | 0.253 | 321 |
| 43 | 1 | 37 | 0.0186 | 0.0263 | 0.33 | 2.67 | 43 | 0.000 | 0.000 | 0 |
| 44 | 37 | 38 | 0.0752 | 0.1066 | 0.33 | 2.67 | 44 | 0.000 | 0.000 | 0 |
| 45 | 38 | 39 | 0.0727 | 0.1030 | 0.33 | 2.67 | 45 | 0.922 | 0.486 | 1,011 |
| 46 | 39 | 40 | 0.0596 | 0.0845 | 0.33 | 2.67 | 46 | 0.308 | 0.162 | 311 |
| 47 | 40 | 41 | 0.0067 | 0.0094 | 0.33 | 2.67 | 47 | 1.217 | 0.641 | 133 |
| 48 | 41 | 42 | 0.0777 | 0.1101 | 0.33 | 2.67 | 48 | 0.000 | 0.000 | 0 |
| 49 | 42 | 43 | 0.0019 | 0.0027 | 0.33 | 2.67 | 49 | 1.626 | 0.856 | 1,309 |
| 82 | 70 | 71 | 0.0665 | 0.0942 | 0.67 | 26 | 82 | 0.681 | 0.359 | 31 |
| 83 | 71 | 72 | 0.0773 | 0.1096 | 0.67 | 26 | 83 | 0.000 | 0.000 | 0 |
| 84 | 71 | 101 | 0.0527 | 0.0747 | 0.67 | 26 | 84 | 0.395 | 0.208 | 10 |
| 85 | 1 | 73 | 0.0000 | 0.0009 | 2.33 | 57.67 | 85 | 0.627 | 0.330 | 6 |
| 86 | 73 | 74 | 0.1192 | 0.1690 | 2.33 | 57.67 | 86 | 0.008 | 0.004 | 1 |
| 87 | 74 | 75 | 0.2825 | 0.4004 | 2.33 | 57.67 | 87 | 0.000 | 0.000 | 0 |
| 88 | 75 | 112 | 0.0085 | 0.0121 | 2.33 | 57.67 | 88 | 0.199 | 0.105 | 288 |
| 89 | 1 | 76 | 0.0000 | 0.0008 | 0.33 | 30 | 89 | 1.470 | 0.775 | 3 |
| 90 | 76 | 77 | 0.1462 | 0.2073 | 0.33 | 30 | 90 | 3.088 | 1.627 | 5,062 |
| 91 | 1 | 78 | 0.0000 | 0.0006 | 3.33 | 62.67 | 91 | 0.000 | 0.000 | 0 |
| 92 | 78 | 79 | 0.1306 | 0.1851 | 3.33 | 62.67 | 92 | 0.287 | 0.151 | 101 |
| 93 | 79 | 80 | 0.0269 | 0.0381 | 3.33 | 62.67 | 93 | 0.828 | 0.436 | 446 |
| Branch No. | Fbus | Tbus | R | X | Failure rate (Times/Year) | Duration Time (Minutes/Year) | Bus No. | P Load (kW) | Q Load (kVar) | No. Customers |
| 95 | 81 | 82 | 0.1166 | 0.1653 | 2.67 | 146.67 | 95 | 1.006 | 0.530 | 258 |
| 96 | 82 | 83 | 0.0010 | 0.0014 | 2.67 | 146.67 | 96 | 0.558 | 0.294 | 205 |
| 97 | 83 | 84 | 0.1114 | 0.1579 | 2.67 | 146.67 | 97 | 0.573 | 0.302 | 336 |
| 98 | 84 | 85 | 0.1880 | 0.2665 | 2.67 | 146.67 | 98 | 0.259 | 0.137 | 426 |
| 99 | 85 | 86 | 0.0339 | 0.0481 | 2.67 | 146.67 | 99 | 0.065 | 0.034 | 85 |
| 100 | 86 | 87 | 0.0021 | 0.0030 | 2.67 | 146.67 | 100 | 0.027 | 0.014 | 42 |
| 101 | 87 | 88 | 0.1180 | 0.1672 | 2.67 | 146.67 | 101 | 2.145 | 1.130 | 1,316 |
| 102 | 88 | 89 | 0.0176 | 0.0249 | 2.67 | 146.67 | 102 | 0.000 | 0.000 | 0 |
| 103 | 89 | 90 | 0.2494 | 0.3534 | 6.67 | 462.67 | 103 | 0.522 | 0.275 | 172 |
| 104 | 1 | 91 | 0.0001 | 0.0020 | 0.67 | 10.33 | 104 | 0.507 | 0.267 | 14 |
| 105 | 91 | 92 | 0.0313 | 0.0444 | 0.67 | 10.33 | 105 | 0.061 | 0.032 | 30 |
| 106 | 92 | 93 | 0.0379 | 0.0537 | 0.67 | 10.33 | 106 | 0.322 | 0.170 | 185 |
| 107 | 93 | 94 | 0.0159 | 0.0579 | 0.67 | 10.33 | 107 | 0.087 | 0.046 | 323 |
| 108 | 94 | 95 | 0.0032 | 0.0046 | 0.67 | 10.33 | 108 | 0.000 | 0.000 | 0 |
| 109 | 95 | 96 | 0.0117 | 0.0165 | 0.67 | 10.33 | 109 | 0.000 | 0.000 | 0 |
| 110 | 96 | 97 | 0.0046 | 0.0065 | 0.67 | 10.33 | 110 | 0.595 | 0.313 | 4 |
| 111 | 94 | 98 | 0.0001 | 0.0012 | 0.67 | 10.33 | 111 | 2.618 | 1.379 | 2,411 |
| 112 | 1 | 102 | 0.0001 | 0.0018 | 3 | 101 | 112 | 0.000 | 0.000 | 0 |
| 113 | 102 | 103 | 0.0623 | 0.0883 | 3 | 101 | 113 | 0.895 | 0.471 | 688 |
| 114 | 103 | 104 | 0.0575 | 0.0814 | 3 | 101 | 114 | 0.000 | 0.000 | 0 |
| 115 | 104 | 105 | 0.0357 | 0.0506 | 3 | 101 | 115 | 1.906 | 1.004 | 3,605 |
| 116 | 105 | 106 | 0.2006 | 0.2844 | 3 | 101 | 116 | 2.811 | 1.481 | 634 |

| | | | | | | | | | | |
|-----|-----|-----|--------|--------|------|--------|-----|-------|-------|-----|
| 117 | 106 | 107 | 0.1658 | 0.2350 | 3 | 101 | 117 | 0.930 | 0.490 | 864 |
| 118 | 107 | 108 | 0.0015 | 0.0022 | 3 | 101 | 118 | 0.057 | 0.030 | 118 |
| 119 | 108 | 109 | 0.0857 | 0.1215 | 3 | 101 | 119 | 1.096 | 0.577 | 383 |
| 120 | 109 | 110 | 0.0825 | 0.1169 | 3 | 101 | 120 | 0.000 | 0.000 | 0 |
| 121 | 109 | 111 | 0.2472 | 0.3504 | 3 | 101 | 121 | 0.067 | 0.035 | 1 |
| 122 | 107 | 112 | 0.0470 | 0.0666 | 3 | 101 | 122 | 0.000 | 0.000 | 0 |
| 123 | 5 | 79 | 0.0592 | 0.0839 | 3.33 | 62.67 | 123 | 0.000 | 0.000 | 0 |
| 124 | 10 | 86 | 0.0296 | 0.0419 | 2.67 | 146.67 | - | - | - | - |
| 125 | 8 | 51 | 0.1267 | 0.1795 | 3.33 | 81.33 | - | - | - | - |
| 126 | 49 | 77 | 0.1475 | 0.2091 | 0.33 | 30 | - | - | - | - |
| 127 | 71 | 94 | 0.0003 | 0.0066 | 0.67 | 26 | - | - | - | - |
| 128 | 98 | 101 | 0.0001 | 0.0012 | 0.67 | 26 | - | - | - | - |
| 129 | 95 | 36 | 0.0457 | 0.0648 | 0.67 | 10.33 | - | - | - | - |
| 130 | 17 | 123 | 0.0144 | 0.0204 | 0.33 | 7.33 | - | - | - | - |
| 131 | 21 | 120 | 0.0000 | 0.0002 | 1.67 | 34.33 | - | - | - | - |
| 132 | 120 | 121 | 0.0174 | 0.0246 | 1.67 | 34.33 | - | - | - | - |
| 133 | 121 | 122 | 0.0000 | 0.0002 | 1.67 | 34.33 | - | - | - | - |
| 134 | 122 | 123 | 0.0144 | 0.0204 | 1.67 | 34.33 | - | - | - | - |
| 135 | 47 | 100 | 0.0138 | 0.0195 | 1.67 | 34.33 | - | - | - | - |
| 136 | 75 | 42 | 0.0757 | 0.1073 | 2.33 | 57.67 | - | - | - | - |
| 137 | 75 | 45 | 0.0736 | 0.1043 | 2.33 | 57.67 | - | - | - | - |
| 138 | 90 | 107 | 0.2646 | 0.3751 | 2.67 | 146.67 | - | - | - | - |
| 139 | 88 | 112 | 0.0473 | 0.0670 | 2.67 | 146.67 | - | - | - | - |
| 140 | 79 | 113 | 0.0187 | 0.0265 | 3.33 | 62.67 | - | - | - | - |
| 141 | 79 | 69 | 0.0265 | 0.0376 | 3.33 | 62.67 | - | - | - | - |
| 142 | 67 | 114 | 0.1145 | 0.1622 | 1.33 | 41.67 | - | - | - | - |
| 143 | 19 | 118 | 0.0125 | 0.0177 | 0.33 | 7.33 | - | - | - | - |
| 144 | 62 | 80 | 0.0269 | 0.0381 | 3.33 | 62.67 | - | - | - | - |